

**METHOD AND MEASURING INSTRUMENT FOR DETERMINING THE
POSITION OF AN EDGE OF A PATTERN ELEMENT ON A SUBSTRATE**

CROSS REFERENCE TO RELATED APPLICATIONS

This invention claims priority of the German patent application 100
5 47 211.7-52 which is incorporated by reference herein.

FIELD OF THE INVENTION

The invention concerns a method and a measuring instrument for
determining the position of an edge to be measured of a pattern element on a
substrate, in which a one-dimensional measured intensity profile is ascertained
10 from a camera image of the edge, and the position of the edge relative to a
reference point is determined therefrom.

BACKGROUND OF THE INVENTION

The pattern elements to be measured are, in particular, opaque or
transparent regions on mask surfaces or patterns on wafers that are used for
15 semiconductor manufacture. The pattern elements to be measured have different
widths and lengths and are distinguishable, for example, by way of the location,
height, and orientation of their edges. In order to indicate the position of a pattern
element on the substrate, often the mutually parallel edge locations are measured
and the position is indicated as the centerline with respect to the two edges. In the
20 case of a pattern element measurable as to width and length, or that of two
intersecting pattern elements, the position is indicated by way of the coordinates
of the intersection point of the two centerlines. Edge position determination is of
particular significance because measurement errors have a direct impact on the

production process. A measurement accuracy on the nanometer scale is therefore demanded by the semiconductor industry.

Measurement of edge positions is accomplished in special coordinate measuring instruments. A measuring instrument suitable for carrying out the known method
5 is described, for example, in the paper of Dr. Carola Bläsing entitled "Pattern Placement Metrology for Mask Making," presented at the Education Program of Semicon Geneva on March 31, 1998.

An example of a typical measuring instrument is described below. The substrate having the pattern element is mounted on a displaceable measurement stage
10 whose position in a measurement plane relative to a reference point can be measured interferometrically. An imaging system is arranged with its optical axis perpendicular to the measurement plane, and images a substrate region having the pattern element onto a detector array in magnified fashion.

The pixels of the detector array are oriented in rows and columns parallel to the
15 axes of an X-Y coordinate system associated with the substrate. The position of the edge of the pattern element is determined, relative to the reference point, in the coordinate system defined on the substrate; the point at which the optical axis of the imaging system strikes the substrate usually serves as the reference point. The detector array is generally oriented in such a way that its center coincides with the
20 reference point. The location of the substrate coordinate system is aligned, using alignment marks, relative to the measurement instrument coordinate system.

Usually the edge of the pattern element to be measured is also oriented parallel or perpendicular to the axes of the mask coordinate system, and thus also to the rows and columns of the detector array.

25 The image, acquired with the detector array, of the pattern element having the edge is analyzed using image-analysis methods. Using a rectangular measurement window generated in software, a specific region of the detector array, i.e. an image

area, is selected for measurement. The measurement window is preferably placed transversely to an edge to be measured of the pattern element.

The contrast level of the edge image varies as a function of the resolution and imaging quality of the imaging system. The best contrast is set using a TV autofocus system. Within a measurement window, the intensities of the pixels lying in one particular row or column parallel to the edge of the pattern element are averaged. This yields an intensity profile of the edge image, perpendicular to the edge, over one row or column of pixels. This intensity profile illustrates the intensity as a function of the location in the measurement direction that is defined perpendicular to the edge.

The location of the edge is defined, for example, by means of a predetermined parameter of the aforesaid intensity profile, for example at 50% of maximum intensity. The interpolated pixel row or pixel column on which the edge is located relative to the reference point is indicated as the resulting edge location. The edge position is thus determined with pixel accuracy.

Determination of the edge location in the calculated intensity profile is of particular importance. In known methods, an edge is assumed to exist in the region of an intensity profile that exhibits a sharp rise or fall in intensity. In this region, a straight-line fit is performed with the individual values of the intensity profile. The problem is that depending on the length of the fitted region and the consequently varying number of individual intensity profile values used for the straight-line fit, the fit can assume different slopes. With different slopes, however, the parameter for determination of the edge position – which is located, for example, at 50% of the maximum intensity – is located at different points, i.e. pixels which correspond to a specific position on the substrate. Calculation of the straight-line fit therefore already constitutes a considerable error in edge determination.

Another problem results from the fact that the measured curve shape of the intensity profile depends, among other factors, on the width and height of the patterns and on the imaging aperture. With optical image acquisition, for example, it is advantageous if the illumination aperture is small compared to the observation
5 aperture. This yields maximum steepness of the intensity profile at the location of the edge, so the position is better defined. Overshoots then occur in the profile, however.

With very narrow patterns, shadow lines of the pattern occur in the intensity profile and supply additional minima that coincide when the pattern lines are
10 particularly narrow (e.g. on wafers). With the straight-line fit method, only the positions of the outer boundaries of the shadow lines can be determined, but a reliable determination of the position of the actual edges of the pattern element is not possible.

US 5,136,661 describes a method for determining edge position. The method
15 defines, for the edge being sought, a straight line with a defined slope. From the image of the pattern, an intensity profile is determined in known fashion, and a measured straight-line fit is calculated therein for each edge contained in it. A variety of evaluation variables are calculated; these are used to select the edge whose measured straight-line fit exhibits the least deviation from the model edge.
20 Selection of the most similar edge is, however, very complex and calculation-intensive. In some cases it requires prior knowledge of the existing pattern widths (e.g. reference widths from the manufacturing process). In addition, the determination of edge position is made with only pixel accuracy, and the problem described above of the straight-line fit on critical intensity profiles remains
25 unresolved.

SUMMARY OF THE INVENTION

It is therefore the object of the invention to describe a method for determining the position of an edge of a pattern element on a substrate which makes possible, on any desired patterned edges, very precise, rapid, and
5 reproducible measurements of the edge position with subpixel accuracy, i.e. to an accuracy of a few nanometers.

This object is achieved by a method for determining the position of an edge to be measured of a pattern element on a substrate in which a one-dimensional measured intensity profile is ascertained from a camera image of the edge and the
10 position of the edge relative to a reference point is determined therefrom; and which according to the present invention is characterized by the following method steps:

- a) ascertaining and storing a complete, nonlinear model intensity profile, which identifies the edge to be measured, of a model edge;
- 15 b) defining with subpixel accuracy a desired model edge position x_k in the model intensity profile;
- c) acquiring a camera image, made up of pixel rows and pixel columns, of the edge to be measured;
- d) 20 placing a measurement window onto the camera image transversely over the edge;
- e) determining from the image signals of the pixels of the measurement window a one-dimensional measured intensity profile of the edge;
- f) identifying the model intensity profile in the measured intensity profile with an indication of its location x_m relative to a reference point; and

- g) determining with subpixel accuracy the position p , referred to said reference point, of the edge to be measured, as $p = x_m + x_k$.

A further object of the invention is to describe a measuring instrument for determining the position of an edge to be measured on a pattern on a substrate with which, on any desired patterned edges, very precise, rapid, and reproducible measurements of the edge position can be performed with subpixel accuracy, i.e. to an accuracy of a few nanometers.

This object is achieved by way of a measuring instrument for determining the position of an edge to be measured of a pattern on a substrate which comprises an incident illumination device, an imaging device, a camera for acquiring a camera image of the edge to be measured, a horizontally X-Y displaceable measurement stage for receiving the substrate, means for placing a rectangular measurement window onto the camera image transversely over the edge, means for determining from the image signals of the pixels of the measurement window a one-dimensional measured intensity profile of the cross section of the edge, and means for determining the position p of the edge relative to a reference point, having the following features:

- a) means for ascertaining and storing a complete, nonlinear model intensity profile, which identifies the edge to be measured, of a model edge;
- b) means for defining with subpixel accuracy a desired edge position x_k in the model intensity profile;
- c) means for identifying the model intensity profile in the measured intensity profile with an indication of its location x_m relative to a reference point; and
- d) means for determining with subpixel accuracy the position p , referred to said reference point, of the edge to be measured, as $p = x_m + x_k$.

The dependent claims recite advantageous embodiments.

5 The invention is based on the idea of employing an edge of the best possible production-engineering quality as a model edge for detecting and measuring further edges of the same type. A model intensity profile of this model edge is generated, and in that profile a desired model edge position x_k is defined with subpixel accuracy. It is also possible to use a mathematically simulated model intensity profile. This can be, for example, a multidimensional fit function to real measured values of the model edge.

10 A camera image is acquired of a substrate having pattern elements whose edges are to be measured. In the camera image, a measurement window is placed (preferably transversely) over an edge to be measured, and a measured intensity profile is determined therefrom.

15 According to the present invention, the model intensity profile is identified in this measured intensity profile and its position x_m relative to a reference point is determined. The model edge position relative to the reference point can thereby also be indicated. It is identical to the desired position $p = x_m + x_k$, relative to the reference point, of the edge to be measured.

20 The method offers the advantage that a determination of the edge position is made only for those edges for whose measured intensity profiles a matching model intensity profile is found. It is thereby possible to measure even substrates, e.g. semiconductor masks, that have differing patterns and differing edge types. For that purpose, the respective characterizing model intensity profiles having the desired model edge positions are ascertained for the various edge types and stored. Upon measurement of the real edges that are to be measured, the particular
25 matching model intensity profile can then be determined and allocated, and the desired positions of all the edges to be measured can be ascertained with subpixel accuracy. This also makes possible automatic measurement of pattern elements on masks or wafers.

In order to identify the model intensity profile in the measured intensity profile, in an advantageous embodiment of the method the model intensity profile is, in mathematical fashion, displaced virtually in one-pixel steps relative to the measurement intensity profile, and a determination is made of the position in
5 which the congruence between the model intensity profile and measured intensity profile is maximal.

For that purpose a correlation value K_j is determined, as an indication of the congruence between the model intensity profile and the measured intensity profile, for all the notional positions x_j assumed in the context of the individual
10 pixel steps. The following formula can be used for determination of the correlation values K_j :

$$K_j = \frac{N \sum_{i=1}^N (P_{i+j} M_i) - \left(\sum_{i=1}^N P_{i+j} \right) \left(\sum_{i=1}^N M_i \right)}{\sqrt{\left(N \sum_{i=1}^N (P_{i+j})^2 - \left(\sum_{i=1}^N P_{i+j} \right)^2 \right) \left(N \sum_{i=1}^N M_i^2 - \left(\sum_{i=1}^N M_i \right)^2 \right)}}$$

in which:

- 15 P = Intensity value of a pixel of the measured intensity profile;
M = Intensity value of a pixel of the model intensity profile;
i = 1 ... N = Pixels of the model intensity profile.

For the respective instantaneous notional position x_j , j indicates that pixel in the measured intensity profile at which the first pixel $i = 1$ of the model intensity
20 profile lies on the measured intensity profile.

The highest correlation value K_j indicates the best congruence. High correlation values K_j can, however, also be generated by noise components of the measured intensity profile if their curve is described by the model intensity profile.

P02250-415203500

According to the present invention, for that purpose the high correlation values K_j that were caused by intensity curves in the noise are excluded from further evaluation.

- 5 The correlation values K_j can be evaluated in various ways. For example, a correlation function $K(x)$ can be prepared from the discrete correlation values K_j , and its maxima can be determined.

- 10 For that purpose, either the correlation curve $K(x)$ itself is examined for maxima, the local maxima caused by noise being rejected. From the remaining maximum x_m associated with the desired edge, the position of the edge to be measured is determined as $p = x_m + x_k$.

Or the derivative $\Delta K(x)$ of the correlation curve $K(x)$ is determined and its zero points are determined, the zero points caused by noise being rejected. From the remaining zero point x_m associated with the desired edge, the position of the edge to be measured is determined as $p = x_m + x_k$.

- 15 It is also possible to evaluate the correlation values directly, i.e. without preparing a correlation curve. This is done by defining a lower limit value for the correlation values that are to be evaluated. For those correlation values that exceed the limit value, at least one local parabolic fit is prepared. If several groups of correlation values lie above the limit value, several parabolic fits are prepared. The local
20 maxima of the parabolic fits are determined with subpixel accuracy. Those local maxima that are caused by intensity curves in the noise are rejected. From the remaining local maximum x_m caused by the edge to be measured, the desired edge position p is determined as $p = x_m + x_k$.

- 25 In another variant of the method, the gradients $\Delta K_j = K_j - K_{j+1}$ are determined for each correlation value K_j . A straight-line fit is then calculated in the vicinity of all possible zero points, the straight-line fit being accomplished in each case with a group of ΔK_j of which at least one value ΔK_j is greater than zero and one less than zero. The zero points of the straight-line fit are determined, and those zero points

that were caused by intensity curves in the noise are rejected. From the remaining zero point x_m that was caused not by the noise but by the edge to be measured, the desired edge position p is determined as $p = x_m + x_k$.

5 In a further embodiment of the method, local parabolic fits are determined in the vicinity of those discrete correlation values K_j whose adjacent correlation values K_{j-1} and K_{j+1} have lower values. The local maxima of the local parabolic fits are determined with subpixel accuracy. Those local maxima that were caused by intensity curves in the noise are then rejected prior to further evaluation. From the remaining maximum x_m that was caused by the edge to be measured, the desired
10 edge position p is determined as $p = x_m + x_k$.

With the method described it is possible to perform a determination, on a pattern element whose right and left edges are mirror images of one another, of the positions of both edges using only one previously known model intensity profile. For example, if a model intensity profile that can identify the left edge is defined,
15 then first the left edge is found using the method already described, and its position is determined with subpixel accuracy. Then the model intensity profile is mirror-reflected so that a second model intensity profile identifying the right edge is formed. With this second model intensity profile, the right edge (which is symmetrical to the left edge) is then found and its position is determined with
20 subpixel accuracy.

Further advantageous applications are evident from the method according to the present invention.

For example, a substrate having multiple edges to be measured can be measured by ascertaining and storing, for different model edges, multiple different nonlinear
25 model intensity profiles which identify the different edge types. In each individual model intensity profile, a desired edge position x_k is defined with subpixel accuracy. At least one measured intensity profile is then ascertained for the substrate having multiple edges to be measured. The various model intensity

profiles are identified in the measured intensity profile; for each model intensity profile found in the measured intensity profile, its position x_m relative to the reference point is indicated. The position p of each edge identified by means of its associated model intensity profile is determined with subpixel accuracy as $p = x_m$
5 $+ x_k$.

In a further embodiment of the method, once again multiple different nonlinear model intensity profiles for different model edges are ascertained and stored. The desired edge position x_k in each individual one of the model intensity profiles is defined with subpixel accuracy. A one-dimensional measured intensity profile is
10 ascertained for a substrate that has an edge to be measured whose model intensity profile was previously determined. The correct model intensity profile associated with the edge to be measured is ascertained from the plurality of previously ascertained model intensity profiles in the measured intensity profile; for the model intensity profile found in the measured intensity profile, its position x_m
15 relative to the reference point is indicated. The position p of the edge identified by means of its associated model intensity profile is calculated with subpixel accuracy as $p = x_m + x_k$.

The method according to the present invention makes it possible to measure the position of the edges of pattern elements even under difficult boundary conditions,
20 for example very narrow patterns or patterns located very close to one another that result in complex measured intensity profiles. Position determination can be made reliably and with subpixel accuracy.

BRIEF DESCRIPTION OF THE DRAWINGS

An exemplary embodiment of the invention will be explained in
25 more detail below with reference to the schematic drawings, in which:

FIG. 1 shows a flow chart of the method according to the present invention;

- FIG. 2 shows a schematic camera image of a pattern element having a model edge;
- FIG. 3 shows a model intensity profile derived from the model edge;
- FIG. 4 shows a model intensity profile with a defined model edge position x_k ;
- 5 FIG. 5 shows a measured intensity profile of a real edge to be measured of a pattern element;
- FIG. 6 shows the position of the identified model intensity profile in the measured intensity profile;
- 10 FIG. 7 shows the determination of the edge position in the measured intensity profile;
- FIG. 8 shows a parabolic fit using discrete correlation values;
- FIG. 9 shows a measuring instrument for determining the position of an edge to be measured of a pattern element on a substrate.

DETAILED DESCRIPTION OF THE INVENTION

- 15 FIG. 1 shows a flow chart of the method according to the present invention. It comprises seven method steps that are described below.

In a first step of the method according to the present invention, a complete, nonlinear model intensity profile, which identifies the edge to be measured, of a model edge is ascertained and stored.

- 20 The model intensity profile can be ascertained in various ways.

One possibility is to measure an intensity profile of a real model edge and take a partial profile area of the measured intensity profile as the model intensity profile.

For that purpose, first a camera image, comprising pixels arranged in rows and columns, is acquired of a model substrate that comprises a model edge whose parameters correspond to those of the edges being measured. The optical measurement parameters used must be the same as those to be used subsequently upon measurement of the edge to be measured that is identifiable by way of the model edge. This ensures that the intensity profiles acquired of identical edges are also identical (or approximately identical).

A rectangular measurement window is placed onto the camera image of the model substrate, and a one-dimensional intensity profile of the model substrate is ascertained from the image signals of the pixels of the measurement window. From this intensity profile, a nonlinear partial profile area that identifies the model edge is taken as the model intensity profile and stored.

In addition, it is possible to prepare a polynomial fit to the model intensity profile thus ascertained, and to use the values of the polynomial fit for calculation of the correlation values K_j .

Another possibility for determining a model intensity profile consists in generating the model intensity profile of the model edge not by measurement, but by mathematical simulation. For example, a polynomial fit to the model intensity profile of the model edge can be prepared, and the values of the polynomial fit used to calculate the correlation values K_j . For the preparation of usable simulation calculations, however, this method requires very accurate knowledge of the edges that are later to be measured, their substrate, and the measurement optics.

In a second step of the method, a desired edge position x_k is defined with subpixel accuracy in the model intensity profile. In other words, the desired edge position can be selected at any desired point in the model intensity profile without consideration of the pixel width. For example, the model intensity profile can be displayed in magnified fashion on a monitor of a computer. The desired edge

position in the model intensity profile can then be arrived at by displacing a cursor and selected, for example by clicking with a computer mouse.

In a third step of the method, a camera image of the edge to be measured, made up of pixel rows and pixel columns, is acquired.

- 5 In a fourth step of the method, a measurement window is placed onto the camera image transversely over the edge. The measurement window defines a portion of the camera image, containing the edge to be measured, from which the one-dimensional measured intensity profile is ascertained. The measurement window can be implemented either with hardware (e.g. by way of an optical or electronic
- 10 window or an image area, or by zooming the camera), or using software. The measurement window is preferably rectangular, and is oriented with its longer side perpendicular to the edge being measured.

- In a fifth step of the method, a one-dimensional measured intensity profile of the edge is determined from the image signals of the pixels of the measurement
- 15 window. A variety of methods, which depend inter alia on the alignment of the measurement window on the substrate or in the camera image, are known for determination of the one-dimensional measured intensity profile.

- For example, if the pixel columns of the measurement window extend in the longitudinal direction of the edge to be measured, determination of a one-
- 20 dimensional measured intensity profile is accomplished in the row direction by adding the column pixel values.

- If, however, the pixel rows of the measurement window extend in the longitudinal direction of the edge to be measured, determination of a one-dimensional measured intensity profile is accomplished in the column direction by adding the
- 25 row pixel values.

In addition, an averaging of the intensity values can be performed when the intensity profile is determined. For example, if the pixel rows of the measurement

window extend in the longitudinal direction of the edge to be measured, determination of a one-dimensional measured intensity profile is accomplished in the column direction by adding and averaging the row pixel values.

- 5 If, however, the pixel columns of the measurement window extend in the longitudinal direction of the edge to be measured, determination of a one-dimensional measured intensity profile is accomplished in the row direction by adding and averaging the column pixel values.

- 10 In a sixth step of the method, the model intensity profile is identified in the measured intensity profile, indicating its location x_m relative to a reference point. For example, the location x_m of the model intensity profile is indicated by the position of the first pixel of the model intensity profile in the measured intensity profile.

- 15 In a variant of the method, for identification of the model intensity profile in the measured intensity profile, the model intensity profile is, for example, displaced in computational fashion in steps, i.e. pixel by pixel, over the measured intensity profile to virtual positions. For each virtual position j , a correlation value K_j is determined as an indication of the quality of the congruence between model intensity profile and measured intensity profile.

- 20 The virtual positions having maximal correlation values may be considered locations at which the model intensity profile is congruent with the measured intensity profile, and from which the position of the edge to be measured can be determined. When the selection is made, those maxima of the correlation values that are caused by noise must be rejected.

- 25 One possibility is to determine a maximum value for the intensity of the noise of the correlation values K_j and to associate with it a correlation limit value K_{min} ; and to reject, before determination of the desired edge position p , those local maxima that lie below that correlation limit value K_{min} .

A further possibility is to determine from the correlation values K_j a correlation function $K(x)$, and to calculate its derivative and the zero points of the derivative. A maximum value for the intensity of the noise of the correlation values K_j is then determined, and a correlation limit value K_{\min} is associated with it. Before
5 determination of the desired edge position p , those zero points whose associated values of the correlation function $K(x)$ lie below that correlation limit value K_{\min} are then rejected.

In a seventh step of the method, the position p of the edge to be measured is determined, as $p = x_m + x_k$, with subpixel accuracy. The position p of the edge is
10 obtained with subpixel accuracy because the position x_k of the model edge in the model intensity profile is defined arbitrarily with subpixel accuracy.

FIG. 2 shows, as an example, a schematic camera image 1 of a model pattern 2 which appears in camera image 1 as two intersecting dark bars against a bright background (i.e. substrate 3). Substrate 3 can be, for example, a wafer or the glass
15 substrate of a semiconductor mask. In this example the left edge of the vertical bar of model pattern 2 is used as model edge 4. A measurement window 5 is arranged transversely to model edge 4 in camera image 1. The camera image is composed of pixels (not depicted) that are arranged in rows and columns.

FIG. 3 shows a model intensity profile, derived from model edge 4 of FIG. 2, that
20 was calculated from the pixels of measurement window 5. The model intensity profile has in the left portion high intensity values that result from the bright background, i.e. substrate 3. In the right portion the model intensity profile has low brightness values that were caused by the vertical dark bar of model pattern 3. In the middle portion, the model intensity profile has a slope, i.e. a decrease in
25 intensity values. The position of model edge 4 lies in the region of this slope. From production parameters of model pattern 3, from previous comparative measurements, and from mathematical considerations, it is now possible to define a reference value for the position of model edge 4.

FIG. 4 shows the model intensity profile of FIG. 3 with such a defined edge position x_k of model edge 4. This is used in the method according to the present invention for determination of the edge position on real edges that have not yet been measured.

- 5 FIG. 5 shows a measured intensity profile that was ascertained on a real edge to be measured of a pattern element. For that purpose, a camera image of the edge to be measured was acquired, and a rectangular measurement window was placed on the camera image transversely over the edge. A one-dimensional measured intensity profile of the cross section of the edge was then calculated from the
10 image signals of the pixels of the measurement window.

- FIG. 6 shows the position x_m of the identified model intensity profile in the measured intensity profile. Stated graphically, for this purpose the model intensity profile was displaced in one-pixel steps over the measured intensity profile, and the location of the greatest congruence was determined. Stated mathematically, a
15 correlation value was determined for each position assumed by the model intensity profile. The position of the model intensity profile in the measured intensity profile then corresponds to the pixel value having the greatest correlation value (correlation value maxima caused by noise already having been left out of consideration).

- 20 FIG. 7 shows for this purpose, as an example, a parabolic fit (shown as a solid line) through discrete correlation values at specific pixels. Each ascertained discrete correlation value is depicted as a small cross. The crosses are therefore arranged at the spacing of the pixels. The maximum of the parabolic fit is determined as the location of the best correlation. The ascertained maximum value
25 K_{\max} of the correlation values lies between two pixels. From the parabolic fit, its position x_m can be determined with subpixel accuracy.

FIG. 8 shows the edge position $p = x_m + x_k$, ascertained according to the present invention, of the edge to be measured in the measured intensity profile. Since the

position x_k of the model edge in the model intensity profile was defined previously, it could be used to find the position p of the actually desired edge.

FIG. 9 shows a measuring instrument 6 for determining the position of an edge to be determined of a pattern element.

- 5 Measuring instrument 6 comprises a granite block 11 that is mounted on vibration dampers 12, 13. On granite block 11, a measurement stage 14 configured as a frame is slidably displaceable in the X and Y directions (indicated in the drawing by two arrows) on air bearings 15, 16. The frame of measurement stage 14 is advantageously made of a glass ceramic with a low coefficient of thermal expansion. The drive elements for displacing measurement stage 14 are not depicted. The position of measurement stage 14 is measured in the X and Y directions with a laser interferometer system 17.

- 10 A mask 18 is set into the frame of measurement stage 14. Mask 18 is made, for example, of quartz glass. Applied on the mask surface is a pattern element 9 having an edge 7 to be measured, whose position is to be determined. Since measurement stage 14 is configured as a frame, mask 8 can also be transilluminated from below.

- 15 Located above mask 18, as the illumination system, is an objective 19 of high optical quality that is adjustable in the Z direction along its optical axis 20 for focusing. Optical axis 20 defines the reference point for measuring the relative position of edge 7.

- 20 By way of a splitter mirror 21, on the one hand the light of an incident-light light source 22 is introduced into the optical beam path, and on the other hand the imaging rays are directed onto a camera 23. Incident-light light source 22 emits, for example, in the near UV spectral region. By means of camera 23, an image of edge 7 of pattern element 8 is acquired, and from it the position of edge 7 is determined as coordinates on mask 18. A CCD camera having a high-resolution pixel array is used, for example, as the camera. Other high-resolution detector

devices can, however, also be used, provided it is possible to determine from their image signals an intensity profile for a measurement window within the camera image.

Set into granite block 11 is a further illumination device that comprises an adjustable-height condenser 24 and a transmitted-light light source 25. The optical axis of condenser 24 aligns with optical axis 20 of objective 19. The light of transmitted-light light source 25 is coupled by means of a coupling-in optical system 26 into an optical waveguide 27. The light emerging from optical waveguide 27 is taken out of optical waveguide 27 by means of a coupling-out optical system 28, and emitted into condenser 24.

The height adjustability of condenser 24 with transmitted-light light source 25 is used to adapt the illuminating beams to be directed onto pattern element 8 to different optical thicknesses of masks 18. The head of condenser 24 can, in particular, extend into the open frame of measurement stage 14. To prevent damage in the context of stage displacements over the entire mask surface, however, condenser 24 can also be withdrawn below the surface of granite block 11. Light sources 22 and 25 can be switched on independently of one another.

Associated with measuring instrument 6 is a computer 29 that is connected to camera 23 and to laser interferometer system 17. A monitor 30 is also connected to computer 29. Monitor 30 serves to display the image acquired with camera 23. A computer program that controls and executes the method steps for measuring the position of edge 7 is installed on computer 29.

The embodiment described above of a measuring instrument for determining the position of edge 7 to be measured offers the possibility of illuminating and measuring with either incident or transmitted light. It is, of course, also possible to equip an apparatus only with an incident-light illumination system or only with a transmitted-light illumination system.

A measurement of the position of edge 7 using measuring instrument 6 will be described below.

Before the actual determination of the position of edge 7 to be measured of pattern element 8, in a first method step firstly a complete, nonlinear model intensity profile, which identifies edge 7 to be measured, of a model edge is ascertained and stored. In the present case an intensity profile of a real model edge of a model pattern (not depicted) was measured, and a partial profile region of the ascertained intensity profile was taken as the model intensity profile.

For that purpose, firstly a camera image, made up of pixel rows and pixel columns, is acquired of the model edge from a model substrate (not depicted) having a model edge. The optical measurement parameters used are the same as those to be used upon measurement of edge 7 to be measured that is identifiable by way of the model edge. The use of the same optical measurement parameters ensures that the intensity profiles acquired of identical edges are also identical (or approximately identical).

The image signals of the camera image are transferred from camera 23 to computer 29. A rectangular measurement window is placed onto the camera image of the model substrate by means of the computer program or by a user. The actual image area can be implemented either with hardware (e.g. by way of an optical or electronic window or an image area, or by zooming the camera), or by means of a computer program, by selecting from the data of the image signals. The measurement window is preferably rectangular, and is oriented with its longer side perpendicular to the edge being measured.

A one-dimensional measured intensity profile of the edge is ascertained by means of the computer program from the image signals of the pixels of the measurement window. From this intensity profile, a nonlinear partial image area that identifies the model edge is taken as the model intensity profile and stored.

In a second step of the method, a desired edge position x_k is defined with subpixel accuracy in the model intensity profile. This can be accomplished by a user, or automatically by means of a function of the computer program in computer 29. The desired ideal edge position can be selected, without consideration of the pixel width, at any arbitrary point on the model intensity profile. For example, the model intensity profile can be displayed in magnified fashion on monitor 30. A user can then arrive at the desired edge position in the model intensity profile by displacing a cursor on monitor 30, and select it, for example by clicking with a computer mouse or another cursor control apparatus (not depicted).

- 10 In a third step of the method, as depicted in the Figure, mask 18 is placed onto measurement stage 14. Camera 23 is then used to acquire a camera image of edge 7 to be measured, made up of pixel rows and pixel columns.

- 15 In a fourth step of the method, a measurement window is placed transversely over the edge in the camera image depicted on monitor 30. The measurement window defines a portion of the camera image containing edge 7 to be measured. As already described with reference to creation of the model intensity profile, the measurement window can be defined by a user or by the computer program.

- 20 In a fifth step of the method, computer 29 calculates from the image signals of the pixels of the selected measurement window, using the computer program, a one-dimensional measured intensity profile of edge 7. The measured intensity profile describes the intensity curve in the camera image of edge 7, transversely to said edge 7.

- 25 In a sixth step of the method, the point in the measured intensity profile at which the model intensity profile appears or is contained is ascertained with computer 29 by means of the computer program. In other words, the model intensity profile is identified and localized in the measured intensity profile. The location x_m of the model intensity profile in the measured intensity profile is determined relative to a reference point, e.g. optical axis 20. For example, the point (indicated by the pixel

value) in the measured intensity profile at which the first pixel of the model intensity profile appears can be indicated as the location x_m of the model intensity profile.

In a seventh step of the method, the position p of the edge to be measured is
5 determined by the computer by means of the computer program. It is obtained by adding the location x_m of the model intensity profile in the measured intensity profile relative to a reference point and the position x_k of the model edge in the model intensity profile, as $p = x_m + x_k$. The position p of the edge is obtained with subpixel accuracy because the selection of the position x_k of the model edge in the
10 model intensity profile was performed arbitrarily with subpixel accuracy.

The present invention was described with reference to exemplary embodiments. It is nevertheless apparent to any person skilled in this art that changes and modifications can be made without thereby leaving the range of protection of the claims recited hereinafter.

PARTS LIST

- | | |
|----|--------------------------------|
| 1 | Camera image |
| 2 | Model pattern |
| 3 | Substrate |
| 4 | Model edge |
| 5 | Measurement window |
| 6 | Measuring instrument |
| 7 | Edge |
| 8 | Pattern element |
| 11 | Granite block |
| 12 | Vibration damper |
| 13 | Vibration damper |
| 14 | Measurement stage |
| 15 | Air bearing |
| 16 | Air bearing |
| 17 | Laser interferometer system |
| 18 | Mask |
| 19 | Objective |
| 20 | Optical axis |
| 21 | Splitter mirror |
| 22 | Incident-light light source |
| 23 | Camera |
| 24 | Condenser |
| 25 | Transmitted-light light source |
| 26 | Coupling-in optical system |
| 27 | Optical waveguide |
| 28 | Coupling-out optical system |
| 29 | Computer |
| 30 | Monitor |